Modelling of reversible novolac type phenolformaldehyde polymerization

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(Received 1 5 January 1 982; *revised 7 April* 1 982)

The reversible polymerization of acid-catalysed phenol and formaldehyde has been modelled through the use of five species A to E. There are two possible mechanisms for the reverse reaction of the polymer formation based upon which two possible kinetic models (1 and 2) have been proposed. These two models arise because during the reverse reaction between these species and water, two possible routes can occur. It has been shown analytically that both these kinetic models would yield identical concentrations of A to E in the reaction mass; only an uncertainity in predicting concentrations of formaldehyde and bound $CH₂OH$ exists. Thus any of these models may be equivalently chosen if the purpose of the simulation is to analyse the product formed. Analysis of the batch reactor under the variation of the ratio of phenol and formaldehyde, $[P]_0/[F]_0$, in the feed shows that the maximum branching in the polymer occurs at a ratio of 0.5 whereas a ratio 1.60 is found to maximize the formation of linear chains. The application of a vacuum to the reaction mass has been modelled to give a constant but lower water concentration. The effect of the vacuum has been examined and is found to give a longer but more branched polymer compared with that for batch reactors with no vacuum.

Keywords Polymerization; novolac; phenol; formaldehyde; model; kinetics

INTRODUCTION

The condensation polymerization of phenol and formaldehyde in the presence of an acid catalyst is known to give an essentially linear polymer with little branching¹. The polymerization reaction has been schematically written as:

$$
(n+2)\bigodot^{OH} + (n+1) \oplus CH_2OH \rightarrow \bigodot^{OH}ICH_2 \rightarrow \bigodot^{OH} CH_2 \rightarrow n \bigodot^{OH} (1)
$$

where Q^+ indicates that the linkage could occur either at the *ortho* or *para* positions. Kinetically, the representation of the polymer formation through equation (1} is not correct because the *ortho* and *para* positions of the phenol exhibit different reactivities. In addition to this, Drumm et *al.*¹ pointed out the phenomena of molecular shielding in novolac formation, where the unreacted internal *orlho* and *para* positions on a given polymer molecule react at lower rates compared with the sites at the ends of the chain.

In our earlier studies^{$2-4$} on the modelling of novolac formation, various reactions were assumed to be completely irreversible. Molecules having at least two phenol rings were defined as polymer chains and the various sites on these chains, where polymerization can occur, were classified as: (a) *ortho* external O_{cT} ; (b) *para* external p_c ; (c) *ortho* internal O_i ; (d) *para* internal p_i . The above external sites are those which lie on the phenyl groups at the chain ends, whereas the internal sites are the remainder of the sites on the polymer chain. These sites were distinguished

because they react with different rate constants. Mass balance equations for these were written using the general kinetics and solved numerically.

The earlier kinetic scheme, however, cannot be modified for the reversible polymerization of phenol formaldehyde. The difficulty arises because the reverse step involves a reaction between water and $a - CH$, bond and the products formed depend on which groups lie on either side of the $-CH_2$ - linkage. An effort was made in this direction⁵ to write down the various types of bond linkages (thus distinguishing them) in the reaction mass, but this increases the number of species required to model the polymerization to thirty, an impractically high value.

In our earlier efforts to model the irreversible resole type polymerization 6.7 , we proposed a kinetic model in which nineteen species were required. It was noted in a recent review⁸ that novolac formation can be equivalently described by the reaction between these nineteen species. Since this is a more detailed version of the earlier model²⁻⁴, an attempt was also made to extend it to describe the reversible novolac formation. An effort along this line, however, runs into difficulty because the reverse step for the formation of some of the species cannot be easily written.

In this paper we present a simple model for reversible novolac formation. We define five species A to E shown in *Table 1.* Here a dash on the benzene ring indicates either a $CH₂$ linkage or the presence of a $-CH₂OH$ group. In the same table, species A to E have been compared with the species defined in the work of Pal $et \, al.^{6.7}$ Various reactions in the reversible polymerization have been written. While writing the reversible step, it was possible to have two possible routes of reaction and therefore there are two possible kinetic models 1 and 2 as shown in *Table* 2.

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Table 1 Structure of various species used for the modelling of reversible novolac formation

Using kinetic models 1 and 2, mass balance equations for species A to E, phenol, formaldehyde and bound $-CH₂OH$ are written and numerically solved. Since these models represent the two asymptotes, the concentrations of these species in actual polymerization would lie between the two limits. The analysis shows that the concentrations of species A to E are identical for both the models whereas the concentrations of formaldehyde and bound $CH₂OH$ are different. This means that either of these models could be used to predict the properties of the polymer formed.

Our earlier studies have shown the importance of unequal reactivity on the conversion and molecular weight distribution⁹⁻¹³. Here we have examined the effect of unequal reactivity on the reversible formation of the novolac. The ratio of phenol to formaldehyde, $[P]_0/[F]_0$, in the feed to the batch reactor shows that the formation of linear chains are maximized at about $[P]_0/[F]_0 = 1.60$. It is interesting to note that the industrially used ratio is $1.67¹$

KINETIC MODEL

To be able to model reversible novolac formation, the various reactions between species A to E given in *Table 1* are given in *Table 2.* In defining these species, the linkages with both CH₂OH and $-CH_2$ have both been denoted by dashed lines on the phenyl rings. In the reaction mass, there are molecules of phenol and formaldehyde in addition to these species. Formaldehyde *exists I* as methylene glycol (OH-CH₂-OH) and the reaction of the OH group gives rise to bound $CH₂OH$ which can further react to give the formation of a bond. Therefore the various forward reactions in *Table 2* have been divided into

reactions of different sites on P and A to E with formaldehyde (F) and bound $CH₂OH$. Since there are two groups on $CH₂(OH)$ ₂, it reacts at twice the rate of reaction of bound $CH₂OH$.

To write a general kinetic scheme accounting for molecular shielding in *Table 2*, four rate constants, k_1 for external *ortho,* k_2 for internal *ortho,* k_3 for internal *para* and k_4 for external *para* sites have been defined. In a given reaction, the overall reactivity is assumed to be completely determined by the site involved. Species A has two external *ort ho* sites and whenever either of them is reacted

(2) Reverse reactions :

Model 2

(1) Forward reactions:

In model 2 forward reactions are same as in model 1 ; only the **reverse** reactions are different.

with F or $CH₂OH$ (reactions (2.1) and (2.8) of *Table 2*), species C is formed. When the reaction with formaldehyde occurs, in addition to the formation of C, a bound CH₂OH group is also produced. Similarly B has one external *ortho* and one external *para* site, C has one internal *ortho* and D has one internal *para* site and their reactions are similarly written.

In the reverse reaction of novolac polymer molecules, water can interact with $-CH_2$ - bonds as well as bound $CH₂OH$ groups. To be able to write the mechanism of reaction of water with bonds, both the endings of the bond must be specified. In model 1 described in *Table 2* the various link points on species A to E have been assumed to be largely CH₂OH. As a result when these react with water, formaldehyde (F) is formed with a loss of a bound CH₂OH group. This fact has been represented in equations (2.15) to (2.20) in *Table 2* as $(F-CH₂OH)$ on their right hand sides. This is done only for the purpose of book-keeping.

In model 2, also given in *Tuble 2,* the various link points have been assumed to be $CH₂$ bonds. Consequently, when A to E react with $H₂O$ in the reverse reaction, the reaction product is essentially $-CH₂OH$. Results for actual polymerizations would lie between these two limits of models 1 and 2. With these kinetic models, the mass balance equations for various species can be written for isothermal batch reactors as follows:

Model 1
\n
$$
\frac{d[A]}{dt} = 2k_4[P][F] - 4k_1[A][F]
$$
\n
$$
+ k_4[P][CH_2OH] - 2k_1[A][CH_2OH]
$$
\n
$$
- k_5[A][H_2O] + k_6[C][H_2O]
$$
\n(2)

$$
\frac{d[B]}{dt} = 4k_1[P][F] - 2k_1[B][F] - 2k_4[B][F] \n+ 2k_1[P][CH_2OH] - k_1[B][CH_2OH] \n- k_4[B][CH_2OH] - k_6[B][CH_2OH] \n+ k_5[C][H_2O] + 2k_6[D][H_2O]
$$
\n(3)

$$
\frac{d[C]}{dt} = 4k_1[A][F] + 2k_4[B][F] - k_2[C][F] \n+ 2k_1[A][CH_2OH] + k_4[B][CH_2OH] \n- k_2[C][CH_2OH] - k_3[C][H_2O] \n- k_6[C][H_2O] + 2k_6[E][H_2O]
$$
\n(4)

$$
\frac{d[D]}{dt} = 2k_1[B][F] - 2k_3[D][F]
$$

+ k₁[B][CH₂OH] - k₃[D][CH₂OH]
- 2k₆[D][H₂O] + k₅[E][H₂O] (5)

 $\overline{\mathbf{C}}$

$$
\frac{d[E]}{dt} = 2k_2[C][F] + 2k_3[D][F] \n+ k_2[C][CH_2OH] + k_3[D][CH_2OH] \n- 2k_6[E][H_2O] - k_5[E][H_2O]
$$
\n(6)

$$
d[F] = -4k_1[A][F] - 2k_1[B][F] - 2k_1[B][F] - 2k_1[B][F] - 2k_2[C][F] - 2k_3[D][F] - 4k_1[P][F] + 2k_4[P][F] + k_5[A][H_2O] + k_6[B][H_2O] + k_5[C][H_2O] + k_6[C][H_2O] + 2k_6[D][H_2O] + 2k_6[E][H_2O] + k_5[E][H_2O]
$$
\n(7)

$$
\frac{d[P]}{dt} = -4k_1[P][F] - 2k_4[P][F] - 2k_1[P][CH_2OH] + k_4[P][CH_2OH] + k_5[A][H_2O] + k_6[B][H_2O]
$$
\n(8)

$$
\frac{d[CH_2OH]}{dt} = 4k_1[A][F] + 2k_1[B][F]
$$
\n
$$
+ 2k_4[B][F] + 2k_2[C][F]
$$
\n
$$
+ 2k_4[P][F] + 4k_1[P][F]
$$
\n
$$
+ 2k_4[P][F]
$$
\n
$$
- 2k_1[A][CH_2OH] - k_1[B][CH_2OH]
$$
\n
$$
- k_4[B][CH_2OH] - k_2[C][CH_2OH]
$$
\n
$$
- k_3[D][CH_2OH] - 2k_1[P][CH_2OH]
$$
\n
$$
- k_4[P][CH_2OH] - k_5[A][H_2O]
$$
\n
$$
- k_6[B][H_2O] - k_5[C][H_2O]
$$
\n
$$
- k_6[C][H_2O] - 2k_6[D][H_2O]
$$
\n
$$
- 2k_6[E][H_2O] - k_5[E][H_2O]
$$
\n
$$
\frac{d[H_2O]}{dt} = 4k_1[A][F] + 2k_1[B][F] + 2k_4[B][F]
$$
\n
$$
+ 2k_2[C][F] + k_3[D][F] + 4k_1[P][F]
$$
\n
$$
2k_4[P][F] + 2k_1[A][CH_2OH]
$$
\n
$$
+ k_1[B][CH_2OH] + k_4[B][CH_2OH]
$$
\n
$$
+ k_2[C][CH_2OH] + k_4[B][CH_2OH]
$$
\n
$$
+ 2k_1[P][CH_2OH] + k_4[P][CH_2OH]
$$
\n
$$
- k_5[A][H_2O] - k_6[B][H_2O]
$$
\n
$$
- k_5[C][H_2O] - k_6[C][H_2O] - 2k_6[D][H_2O]
$$

Model 2

For this kinetic model, only the reverse terms of the mass balance equations of F and $CH₂OH$ change. The mass balance equations of other species are the same as for model 1.

$$
\frac{d[F]}{dt} = -4k_1[A][F] - 2k_1[B][F] \n- 2k_4[B][F] - 2k_2[C][F] \n2k_3[D][F] - 4k_1[P][F] \n- 2k_4[P][F]
$$
\n(11)

 $-2k_6[E][H_2O]-k_5[E][H_2O]$ (10)

$$
d[CH2OH] = 4k1[A][F] + 2k1[B][F]+ 2k4[B][F] + 2k2[C][F]+ 2k3[D][F] + 4k1[P][F]+ 2k4[P][F] - 2k1[A][CH2OH]+ k4[B][CH2OH] - k4[B][CH2OH]- k2[C][CH2OH] - k3[D][CH2OH]- 2k1[P][CH2OH] - k4[P][CH2OH]+ k5[A][H2O] + k6[B][H2O]+ k5[C][H2O] + k6[C][H2O]+ k5[C][H2O] + 2k6[E][H2O]+ k5[E][H2O] (12)
$$

Equations (2) to (12) were rearranged and written in terms of the following dimensionless groups:

$$
x = k_1 t [F]_0
$$

\n
$$
R_1 = k_2/k_1; R_2 = k_3/k_1; R_3 = k_4/k_1;
$$

\n
$$
R_4 = k_5/k_1; R_5 = k_6/k_1
$$

\n
$$
y_1 = [A]/[F]_0
$$

\n
$$
y_2 = [B]/[F]_0
$$

Equations (2) to (12) are coupled nonlinear differential equations and are solved using the Runge-Kutta method of fourth order with Δx as 10^{-3} .

RESULTS AND DISCUSSION

To check the numerical stability of the solution, the time increment Δx was changed from 10^{-3} to 10^{-5} and the same concentration profiles of the various species were obtained. In addition to this, in all computations, the ring count defined by

Ring count =
$$
[P] + [A] + [B] + [C] + [D] + [E]
$$
 (13)

was calculated. This should remain constant, which was indeed found to be so in all computations.

Our earlier studies have shown that the irreversible formation of novolac is insensitive to the phenomena of molecular shielding. As a result, the following approximation has been made in this simulation study

$$
R_1 = 1 \tag{14a}
$$

$$
R_2 = R_3 \tag{14b}
$$

In addition to this, the reverse step involves two rate constants, k_5 to k_6 . Since the *ortho* and *para* positions in the forward reaction exhibit different reactivities, they are assumed to differ in the reactivity by the same ratio in the reverse step. This would mean that

$$
\frac{R_4}{R_5} = R_3 \tag{15}
$$

In the absence of any information on the equilibrium of phenol formaldehyde polymerization, R_5 has been taken as a parameter in this study. The concentrations of species A to E, phenol, formaldehyde, bound CH₂OH and water have been calculated for models 1 and 2 for various values of R_5 . It was found that for both these models, [A], [B], $[C]$, $[D]$, $[E]$, $[P]$ and $[H₂O]$ *versus* time remained the same for any given set of rate constants. This appears to be surprising on the first hand. It may be noted that models 1 and 2 differ only in the reverse reactions and the terms in the balance equations for $\lceil CH, OH \rceil$ and $\lceil F \rceil$ are different for these two models. For other species, however, the change in the model is supposed to have an indirect effect through the concentrations of F and $CH₂OH$ in the reaction mass. It is further observed that whenever a functional group OH reacts, one molecule of water is formed. As a result, at any time of polymerization, the following relation would hold:

$$
2[F] + [CH2OH] + [H2O] = 2[F]0 (16)
$$

where the feed to the reactor is assumed to be a mixture of $[P]_0$ moles of phenol and $[F]_0$ moles of formaldehyde only. In equations (2) to (10), the terms involving concentrations of formaldehyde and bound CH₂OH always appear together as $(2[**F**] + [CH₂OH])$. Through equations (7) and (8) for model 1 and equations (11) and (12) for model 2, it can be shown that the rate of change of $(2[F] + [CH, OH])$ is the same for both the models.

In our earlier model of irreversible novolac, formation, we had used the various reaction sites $(O'_e, O_e, O_i$ and p_e) on polymer chains having chain length of two units and more. The results presented therein cannot be directly compared with the results obtained here for irreversible polymerization because in models 1 and 2 we have included species of unit chain length (excluding phenol) as polymer molecules. On adding concentrations of

to the results of various site concentrations obtained from the earlier studies^{$2,3$}, results of this work are found to be consistent.

In *Figures 1* to 7, y_1 to y_7 have been plotted as a function of the dimensionless time, x, with R_5 as parameter. $(2[A] + [B])$ gives the total concentration of external *ortho* sites in the reaction mass and has been plotted in *Figure 1.* For a given R_5 , the curve rises very quickly but falls only very slightly at longer times. As R_5 is increased from 0.0 to 1.0, the change in these curves is only very slight; however for values of R_5 higher than this, the fall in the numerical value is large indicating that the polymerization has not proceeded to any extent. A similar fall in C *versus x* in *Figure 2, D versus x* in *Figure 3* and E *versus x* in *Figure 4* confirms the decrease in chain length of the polymer formed as R_5 is increased to a large value. As shown in *Figure 5,* the asymptotic value of unreacted phenol in the reaction mass with R_5 increases accordingly. In our earlier studies of irreversible formation, we found that the concentrations of various sites first increased reaching an asymptotic value for large times. This behaviour was found to be so because all the formaldehyde and bound $-CH,OH$ are completely reacted. In the reversible novolac formation, we find the same behaviour, except for the fact that the curves reach the asymptotic value because of the equilibrium. As R_5 is increased, the polymer formation reduces and the asymptotic values for curves for [A] to [El *versus x* fall.

Figure 1 Effect of R_5 on (2[A] + [B]) versus x. $R_1 = 1$. $R_2 =$ $R_3 = 2.4$, $R_4 = 2.4$ R_5 , $[P]_0/[F]_0 = 1.67$

Figure 2 Effect of R_5 on [C] *versus x.* $R_1 = 1$, $R_2 = R_3 = 2.4$, $R_4 = 2.4 R_5$, $[P]_0/[F]_0 = 1.67$

Figure 3 Effect of R_5 on [D] *versus x.* $R_1 = 1$, $R_2 = R_3 = 2.4$, $R_4 = 2.4 R_5$, $[P]_0/[F]_0 = 1.67$

The concentrations of formaldehyde and bound CH2OH *versus* **dimensionless time x for both models 1 and 2 are given in** *Figures 6* **and 7 respectively. For model 1, [F] approaches an asymptotic value for large values x,** which increases as \mathbb{R}_5 is increased; for Model 2, however, as expected, the effect of R_5 is very small. In *Figure 7,* [CH, OH] has been plotted as a function of x and is found **to undergo a maximum before going to zero for longer** times. For model 1, the maximum value of $[CH₂OH]$ **reduces whereas for model 2, the maximum disappears for** values of R_5 greater than 1.

In *Figures 8* **to** *11,* **the effect of the phenol to for**maldehyde ratio in the feed, $[P]_0/[F]_0$, on the concentration of various species has been examined. These computational runs were made with $[F]_0 = 1$ and varying **[P]o** in the feed. Thus the upward increasing trend in *Figure 8* for (2[A] + [B]) with increasing $[P]_0/[F]_0$ exists because more and more phenol molecules give a larger number of external *ortho* sites. A similar trend in [C] and [D] is found in *Fiqures 9* and 10 respectively. However for $[P]_0/[F]_0$ beyond 1.6, both $[C]$ and $[D]$ begin to fall. It may be noted that the increase in $[C]$ and $[D]$ indicates the increase in linear polymer molecules of chain length of 3 units and more. Thus $[P]_0/[F]_0 = 1.60$ maximizes the formation of linear chains. It is interesting to note that commercial novolac reactors are opcratcd at the feed ratio of 1.67. In *Figure 11*, the effect of $[P]_0/[F]_0$ in the feed on [El *rersus x* has been examined. As this ratio is increased, [E] *rersus x* curves rise to higher values and for the ratio beyond 0.5 it begins to fall. A large concentration of species E in the reaction mass indicates that the

Figure 4 Effect of R_5 on E versus x. $R_1 = 1$, $R_2 = R_3 = 2.4$, $R_4 = 2.4 R_5$, $[P]_0 / [F]_0 = 1.67$

Figure 5 Effect of R_5 on [P] *versus x.* $R_1 = 1$, $R_2 = R_3 = 2.4$, R_4 = 2.4 R_5 , $[P]_0/[F]_0$ = 1.67

Figure 6 Effect of R_5 on [F] *versus x* for model 1 and 2. $R_1 = 1$, $R_2 = R_3 = 2.4$, $R_4 = 2.4$, R_5 , $[P]_0/[F]_0 = 1.67$

Figure 7 Effect of R_5 on [CH₂OH] *versus x* for models 1 and 2. $R_1 = 1$, $R_2 = R_3 = 2.4$, $R_4 = 2.4$ R_5 , $[P]_0/[F]_0 = 1.67$

polymer formed is branched. This would mean that $[P]_0/[F]_0=0.5$ would lead to the highest branching which is consistent with our earlier studies of resole formation^{6,8}. Indeed, resole polymerizations are usually carried out at these values of $[P]_0/[F]_0$.

In the computation of *Figures 1* to *11*, the water as the condensation product is assumed to remain in one phase during the polymerization. When a vacuum is applied on the reaction mass, the water concentration falls and the rate of polymerization is expected to increase. A concentration profile of water is established which can, in general, be solved through differential mass transfer equations^{14,15}. For most applications where the gel point is not reached, the mass transfer resistance is small, as a result of which, the concentration of water can be assumed to be uniform in the reaction mass given by the vapour liquid equilibrium existing at the pressure applied ^{16.17}. In *Figures 12* to *14,* we have considered the concentration of water in the reaction mass as a parameter and compared the results with the results of batch reactors where water is

not removed. In *Figures 12, 13* and *14*, the effect of [H,O] level (i.e., the vacuum applied) on $(2[A] + [B])$, $[C]$ and [E] *versus x* has been examined. As the concentration level of $H₂O$ is reduced, these curves shift upwards; however, the effect on $(2[A] + [B])$ *versus x* is relatively small. For the same residence time, on application of a vacuum, this means that the branching and the length of the polymer formed is increased.

CONCLUSION

Reversible novolac formation has been modelled through the five reactive species A to E. These differ from each other only in terms of their reacted sites. A given site on

Figure 8 Effect of $[P]_0/[F]_0$ on $(2[A] + [B])$ *versus x.* $R_1 = 1$, R_2 = R₃ = 2.4, R₄ = 0.24, R₅ = 0.1

Figure 9 Effect of $[P]_0/[F]_0$ on $[C]$ *versus x.* $R_1 = 1$, $R_2 = R_3 =$ 2.4, R_4 = 0.24, R_5 = 0.1

Figure 10 Effect of $\left[P\right]_0/\left[F\right]_0$ on [D] *versus x. R* $_1$ = 1, *R* $_2$ = *R* $_3$ = 2.4, $R_4 = 0.24$, $R_5 = 0.1$

Figure 11 Effect of $[P]_0/[F]_0$ on *E versus x.* $R_1 = 1$, $R_2 = R_3 =$ 2.4, R_4 = 0.24, R_5 = 0.1

these species could either be connected through a $-CH$, bond or just be simply linked to a CH₂OH group.

Depending upon whether the linkages on species A to E are predominantly $-CH$, bonds of CH, OH, it is possible **to write two asymptotic kinetic models 1 and 2. The analysis of these models show that both predict identical characteristics of the polymer formed whereas an un**certainty exists in predicting [F] and [CH₂OH] in the **reaction mass.**

For predicting the nature of the polymer formed, either of the models 1 and 2 could be chosen to examine the effect of reverse rate conslant and the ratio of phenol and formaldehyde, $[P]_0/[F]_0$, model 1 has been used for the **analysis. Our earlier analyses have shown that molecular shielding has only a very small influence on the character-**

and external *ortho* **and** *paru* **sites have not been disti-** $[P]_0/[F]_0 = +6$ **i nguished kinetically here. In the reverse reaction the** *para* **O~ra 14 I 2 I 8 20< - linkages are assumed to react with water with higher rate** constants compared with that for *ortho* linkages. The effect of **increasing the reverse rate constant is to reduce the polymer chains, as expected.**

increased branching which undergoes a maximum at $[P]_0/[F]_0 \approx 0.5$. When this ratio is increased further, the degree of branching falls but, the concentrations of OO4- *III///* internal sites (whose measure is indicated by [C] and [D]) **in the reaction** mass undergoes a maximum at

Figure 12 Effect of vacuum on $(2[A] + [B])$ versus x. $R_1 = 1$, $R_2 = R_3 = 2.4$, $R_4 = 0.24$, $R_5 = 0.1$, $[P]_0/[F]_0 = 1.67$

Figure 13 Effect of vacuum on [C] *versus x. R*₁ = 1, *R*₂ = *R*₃ 2.4, R_4 = 0.24, R_5 = 0.1, $[P]_0/[F]_0$ = 1.67

Figure 14 Effect of vacuum on [E] *versus x.* $R_1 = 1$, $R_2 = R_3 =$ 2.4, $R_4 = 0.24$, $R_5 = 0.1$, $[P]_0/[F]_0 = 1.67$

 $[P]_0/[F]_0 = 1.60$. This maximum in [C] and [D] implies the preponderance of linear polymer chains with chain lengths of 3 units and more. Interestingly enough, industrially, reactors producing novolac polymer, where the aim is to maximize the production of linear chains, are operated with $[P]_0/[F]_0 = 1.67$.

The effect of application of vacuum on the novolac polymer formed has also been examined by assuming a constant water concentration in the reaction mass. As water is reduced through the application of vacuum, a longer and more highly branched polymer is formed.

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